



S99TC01-2112

# **User Manual**

Ball Spline SP-01-0-EN-2204-MA

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# 1 Introduction of Ball Splines

# 1.1 Linear ball splines

• Cylinder type (RS type)





• Rotary type (FSR type)



#### 1.1.1 Product structure

Fig. 1.1: Product structure diagram of the linear ball spline



#### 1.1.2 Features

The HIWIN ball spline is a rolling guide component consisting of a spline nut, a spline shaft, a steel ball and a retainer. Rolling the steel ball in an infinite rolling cycle between the spline nut and the spline shaft allows the spline nut to move linearly along the spline shaft with high precision. The steel ball on the ball spline is of angular contact structure and can withstand radial loads and torsional loads. The spline nut and the outer ring are designed as one piece, which enables the ball spline to achieve a simplified structure.

The ball spline is equipped with 3 sets of balls in a face-to-face angular contact design. The balls are continuously moved in a complete cycle by means of a steel ball retainer. The optimized design of the retainer enables the guidance with high speed, high acceleration and deceleration. In addition, the encapsulation of the ball by the retainer makes it possible to withdraw the spline nut from the spline shaft without the balls falling out.

Transmittable torque capacity

Compared with linear bearings, the ball in the rolling groove is in angular contact, so the spline nut and the spline shaft can move in relation to each other to achieve the function of transmitting torque.

- One-piece structure The spline nut and the outer ring are made in a one-piece structure to achieve high precision and compact design.
- Easy to install

The ball spline retainer prevents the balls from falling out even if the spline shaft is removed from the spline nut.

Lubricant circuit

By optimizing the design of the lubricant circuit, the lubrication grease is directed to where the balls circulation to improve the lubrication effect and increase the service life.

### 1.2 Compound ball splines

• Ball screw spline (FBR type)



#### 1.2.1 Product structure

Fig. 1.2: Product structure diagram of the compound ball spline



#### 1.2.2 Features

The compound ball spline consists of a ball spline nut, a ball screw nut, a spline shaft, steel balls and retainers. Through the interaction of the two nuts on the spline, three modes of operation (linear, rotary and helical), can be integrated on one shaft.

# 2 Description of ball spline specifications

# 2.1 Description of specifications - RS, FS, FSR

Table 2.1: Order code RS, FS, FSR

Numb	er	1	-	2	-	3	4	-	5	-	6	-	7	-	8
Code		SP	-	20	-	2	FS	-	400	-	500	-	C	-	S
1	SP	Colle	ctive na	ame fo	r ball s	pline p	roduct	s							
2	20	Spline	e shaft	outer	diamet	er									
3	2	Numb 1pcs	oer of s withou	pline n t mark	uts on ing	1 shaf	t:								
4	FS	Nut ty RS: FS: FSR:	/pe: Cylindo Flange Rotary	er type type type											
5	400	Lengt (Unit	:h of st mm)	raight	groove										
6	500	Total (Unit	length mm)	of spli	ne sha	ft									
7	C	Accur C: H: P:	racy: Norma High g Precisi	l grade rade ion gra	e de										
8	S	Spline S: None	e shaft S	markir Solid sł łollow	ng: naft shaft										

#### Table 2.2: Order code FBR, FBL

Numb	er	1	-	2	-	3	-	4	-	5	-	6
Code		SP	-	20	-	FBR	-	400	-	500	-	S
1	SP	Collecti	ve name	for ball	spline pr	oducts						
2	20	Spline s	haft out	er diame	ter							
3	FBR	Nut type FBR: Ri FBL: Le	e: ght rotat eft rotati	tion on								
4	400	Length (Unit m	of straig m)	ht groov	e							
5	500	Total le (Unit m	ngth of s m)	spline sh	aft							
6	S	Spline s S: None:	haft ma Solic Holle	rking I shaft ow shaft								

# 3 Selecting procedure of ball spline

#### 3.1 Diagram of the procedure for selecting the ball spline



#### 3.2 Strength design of spline shaft

The ball spline shaft is a composite shaft capable of withstanding radial loads and torsions. In case of high loads or torsions, it is necessary to take into account the strength of the spline shaft.

#### 3.2.1 Spline shaft subjected to bending

When bending moments act on the spline shaft of the ball spline, the most suitable spline diameter can be calculated according to the following Formula 3.1.

Formula 3.1

 $M = \sigma \times Z$  and  $Z = \frac{M}{\sigma}$ 

- M: Maximum torque acting on spline shaft (Nmm)
- σ: Allowable bending stress of spline shaft (98 N/mm<sup>2</sup>)
- Z: Coefficient of the cross-section of the spline shaft (5,77x10<sup>2</sup> mm<sup>3</sup> for specification SP20)

Fig. 3.1: Schematic diagram of splines subjected to bending moments



#### 3.2.2 Spline shaft subjected to torsion

When torsions act on the ball spline shaft, the most suitable spline diameter can be calculated according to the following Formula 3.2.

Formula 3.2

$$T = \tau_a \times Z_p$$
 and  $Z_p = \frac{T}{\tau}$ 

- T: Maximum torque (Nmm)
- $\tau_a$ : Allowable stress on the spline shaft (49 N/mm<sup>2</sup>)
- $Z_p$ : Coefficient of the polar cross-section of the spline shaft (specification 20 is 1,15 x 103 mm<sup>3</sup>)

Fig. 3.2: Schematic diagram of splines subjected to torques



#### 3.2.3 Spline shaft subjected to bending and torsion simultaneously

When the spline shaft of a ball spline is subjected to both bending moment and torque, the diameter of the spline shaft shall be calculated separately, with the equivalent bending moment ( $M_e$ ) and equivalent torque ( $T_e$ ) taken into account and the larger outer diameter of the spline shaft is taken as the diameter of the spline shaft.

Equivalent bending moment:

Formula 3.3

$$\begin{split} M_e &= \frac{M + \sqrt{M^2 + T^2}}{2} = \frac{M}{2} \Biggl\{ 1 + \sqrt{1 + \left(\frac{T}{M}\right)^2} \Biggr\} \\ M_e &= \sigma * Z \end{split}$$

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Equivalent torque:

Formula 3.4

$$\begin{split} T_{\rm e} &= \sqrt{M^2 + T^2} = M \times \sqrt{1 + \left(\frac{T}{M}\right)^2} \\ T_{\rm e} &= \tau_{\rm a} \times Z_{\rm p} \end{split}$$

#### 3.2.4 Stiffness of the spline shaft

Stiffness of the spline shaft is indicated by the torsional angle of the spline shaft of length 1 m, which is limited to about 0,25°.

Formula 3.5

$$\theta = 57,3 \times \frac{T \times L}{G \times I_p}$$

 $\label{eq:Stiffness} \text{Stiffness of the spline shaft} = \frac{\text{Torsional angle}}{\text{Unit length}} = \frac{\theta \times 1.000}{\text{L}} < \frac{1^{\circ}}{4}$ 

Fig. 3.3: Schematic diagram of stiffness of the spline shaft



- Θ: Torsional angle (°)
- L: Length of spline shaft (mm)
- G: Transverse coefficient of elasticity (7,9 x 104 N/mm<sup>2</sup>)
- I<sub>p</sub>: Polar moment of inertia (specification 20 is 1,14 x 104 mm<sup>4</sup>)

#### 3.2.5 Bending and bending angle of the spline shaft

The calculation table of the bending and bending angle of the spline shaft of the ball spline is based on the calculation formula suitable for its stress conditions.



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 $\delta_{max}$ : Maximum bending (mm)

- M<sub>0</sub>: Torque (Nmm)
- I: Span moment (mm)
- I: Geometric moment (mm<sup>4</sup>)
- *i*<sub>1</sub>: Bending angle at support point
- *i*<sub>2</sub>: Bending angle at support point
- P: Concentrated load (N)
- p: Uniform load (N/mm)
- E: Longitudinal coefficient of elasticity 2,06 x 105 (N/mm<sup>2</sup>)

#### 3.2.6 Section characteristics of spline shafts

Nomi	nal diameter	l: Geometric moment mm <sup>4</sup>	Z: Cross-section coefficient mm <sup>3</sup>	lp: Polar moment of inertia mm <sup>4</sup>	Zp: Coefficient of the polar cross- section mm
13	Solid shaft	1,32 x10 <sup>3</sup>	2,09 x10 <sup>2</sup>	2,7 x10 <sup>3</sup>	4,19 x10 <sup>2</sup>
	Hollow shaft	1,29 x10 <sup>3</sup>	2,00 x10 <sup>2</sup>	2,63 x10 <sup>3</sup>	4,09 x10 <sup>2</sup>
16	Solid shaft	3,09 x10 <sup>3</sup>	3,90 x10 <sup>2</sup>	6,18 x10³	7,80 x10 <sup>2</sup>
	Hollow shaft	2,37 x10 <sup>3</sup>	2,99 x10 <sup>2</sup>	4,74 x10 <sup>3</sup>	5,99 x10 <sup>2</sup>
20	Solid shaft	7,61 x10 <sup>3</sup>	7,67 x10 <sup>2</sup>	1,52 x10 <sup>4</sup>	1,53 x10³
	Hollow shaft	5,72 x10 <sup>3</sup>	5,77 x10 <sup>2</sup>	1,14 x10 <sup>4</sup>	1,15 x10 <sup>3</sup>
25	Solid shaft	1,86 x10 <sup>4</sup>	1,50 x10 <sup>3</sup>	3,71 x10 <sup>4</sup>	2,99 x10 <sup>3</sup>
	Hollow shaft	1,34 x10 <sup>4</sup>	1,08 x10 <sup>3</sup>	2,68 x10 <sup>4</sup>	2,16 x10 <sup>3</sup>
32	Solid shaft	5,01 x10 <sup>4</sup>	3,15 x10 <sup>3</sup>	9,90 x10 <sup>4</sup>	6,27 x10 <sup>3</sup>
	Hollow shaft	3,64 x10 <sup>4</sup>	2,29 x10 <sup>3</sup>	7,15 x10 <sup>4</sup>	4,53 x10 <sup>3</sup>

#### Table 3.2: Characteristics of the spline shaft cross-section

#### 3.2.7 Critical velocity of the spline shaft

When the ball spline shaft is rotated by the transmitting power, if the rotation speed of the spline shaft increases to approach the resonance point, the spline cannot move. Therefore, the maximum rotation speed must be limited below the critical velocity without resonance. The critical velocity can be obtained from the following <u>Formula 3.6</u>. (The safety coefficient is considered to be 0,8.) Above the resonance point, or in case of use near the resonance point, the diameter of the spline shaft must be reviewed.

Critical velocity

Formula 3.6

$$N_{c} = \frac{60\lambda^{2}}{2\pi \times l_{b}^{2}} \times \sqrt{\frac{E \times 10^{3} \times I}{\gamma \times A}} \times 0.8$$

 $N_c$ : Critical velocity (min<sup>-1</sup>)

I<sub>b</sub>: Distance between: installation surfaces (mm)

E: Longitudinal modulus of elasticity (2,06 x 10<sup>5</sup> N/mm<sup>2</sup>)

I: Minimum geometric moment of the shaft (mm<sup>4</sup>)

 $\gamma$ : Density (specific center of gravity) (7,85 x 10<sup>s</sup> kg/mm<sup>3</sup>)

A: Area of the end face of the spline shaft (mm<sup>2</sup>)

 $\lambda$ : Dependent on the installation method

1 Fixed - Not fixed,  $\lambda = 1,875$ , as in Fig. 3.4.

2 Supported - Supported,  $\lambda = 3,142$ , as in Fig. 3.5.

3 Fixed - Supported,  $\lambda$  = 3,927, as in Fig. 3.6.

4 Fixed - Fixed,  $\lambda$  = 4,73, as in Fig. 3.7.

Fig. 3.4: Schematic diagram of spline shaft fixed - free





Fig. 3.5: Schematic diagram of spline shaft supported - supported



Fig. 3.6: Schematic diagram of spline shaft fixed - supported



Fig. 3.7: Schematic diagram of spline shaft fixed - fixed



#### 3.3 Predicting life

#### 3.3.1 Rated life

The life of a ball spline can vary considerably even if it is manufactured from the same batch and used under the same motion conditions. Therefore, as a basis for calculating the life of a linear motion system, use the rated life as defined below.

The rated life is the total running distance that can be achieved by having a batch of identical linear motion systems moving separately under the same conditions, 90% of which do not show metal fatigue.

Fig. 3.8: Schematic diagram of the ball spline subjected to stress



The running of the ball spline can be divided into three types of torsions, radial loads and moments. The respective rated life can be obtained according to Formula 3.7 to Formula 3.10. (The basic rated load in each direction of load is recorded in the dimension table of each model number.)

When subjected to torque load

Formula 3.7

$$L = \left(\frac{f_{\rm T} \times f_{\rm C}}{f_{\rm W}} \times \frac{C_{\rm T}}{T_{\rm C}}\right)^3 \times 50$$

• When subjected to radial load

Formula 3.8

$$\mathbf{L} = \left(\frac{\mathbf{f}_{\mathrm{T}} \times \mathbf{f}_{\mathrm{C}}}{\mathbf{f}_{\mathrm{W}}} \times \frac{\mathbf{C}}{\mathbf{T}_{\mathrm{C}}}\right)^{3} \times 50$$

- L: Rated life (km)
- C<sub>T</sub>: Basic dynamic rated torque (Nm)
- T<sub>c</sub>: Calculated value of applied torque (Nm)
- C: Basic dynamic rated load (N)
- P<sub>c</sub>: Calculated value of radial load (N)
- f<sub>T</sub>: Temperature coefficient (see the table)
- f<sub>c</sub>: Contact coefficient (see the table)
- f<sub>w</sub>: Load coefficient (see the table)
- When subjected to both torsional and radial loads simultaneously When subjected to both torsional and radial loads simultaneously, the equivalent radial load can be calculated according to the following <u>Formula 3.9</u> and then the life can be calculated.

Formula 3.9

 $P_{E} = P_{C} + \frac{4T_{C} \times 10^{3}}{i \times dp \times cos\alpha}$ 

P<sub>E</sub>: Equivalent radial load (N)

 $\cos\alpha$ : Contact angle (FBR type  $\alpha$ =70°)

- i: 3 rows of steel balls under load for specification 20
- dp: Ball center diameter (mm)
- Calculating life time

After calculating the rated life (L) using the above formula, the life time can be calculated according to the following Formula 3.10 when the number of strokes and times are fixed.

Formula 3.10

 $L_{\rm h} = \frac{L \times 10^3}{2 \times l_S \times n_1 \times 60}$ 

- L<sub>h</sub>: Life time (h)
- I<sub>s</sub>: Stroke length (m)
- n<sub>1</sub>: Cycles per minute (min<sup>-1</sup>)

#### 3.3.2 f<sub>T</sub>: Temperature coefficient

When using a ball spline in operating temperatures exceeding 100°C, multiply the temperature coefficient of Figure 3-6 when calculating the life, taking into account the adverse effects caused by high temperatures. Also, note that it is necessary to use ball spline products suitable for high temperatures.

#### Note:

In case of operating above 80°C, the material of the gasket and retainer must be changed to a material for the high-temperature specification accordingly.





#### 3.3.3 f<sub>c</sub>: Contact coefficient

When multiple nuts are mounted closely and working in linear motion, it is difficult to get a uniform distributions of loads due to the moment load and mounting accuracy. Therefore when using multiple nuts closely, multiply the basic rated load(C) and (C0) by corresponding contact coefficients in Table 3.3.

	Table 3	3.3:	Contact	coefficient	$(\mathbf{f}_{c})$
--	---------	------	---------	-------------	--------------------

Number of spline nut mounted closely	Contact coefficient f <sub>c</sub>
2	0,81
3	0,72
4	0,66
5	0,61
Usual use	1,00

#### Note:

If the load is expected to be nonuniform in large installations, please refer to the contact coefficients in <u>Table 3.3</u>.

#### 3.3.4 f<sub>w</sub>: Load coefficient

Most machines will have vibration and shock during operation. Vibration is generated during high-speed movement. Shock is caused by frequent starting and stopping. It is very difficult to calculate all correctly. Therefore, when the actual load on the linear motion system is not available, or when the effects of velocity and vibration are significant, please divide the basic rated load (C) and (C0) by the load coefficients obtained from experience in <u>Table 3.4</u>.

Table 3.4:	Loadcoefficient	$(f_w)$
------------	-----------------	---------

Vibration/shock	Velocity V (m/s)	Load coefficient f <sub>w</sub>
Low	Mini speed per hour $V \leq 0,25$	1 ~ 1,2
Small	At low speed $0.25 < V \leq 1$	1,2 ~ 1,5
Medium	At medium speed 1 < V $\leq 2$	1,5 ~ 2
High	At high speed $V > 2$	2 ~ 3,5

#### 3.3.5 Shape of the spline shaft cross-section

Fig. 3.10: Diagram of the ball spline cross-section





Nominal shaft diameter: 13mm or less

Nominal shaft diameter: 16mm or more

#### 3.3.6 Shape of the hollow spline shaft cross-section



Fig. 3.11: Diagram of the hollow ball spline cross-section



Nominal shaft diameter: 13mm or less

Nominal shaft diameter: 16mm or more

Table 5.5. Furtherers of the spline shart cros	ss-section
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Nominal shaft diameter	13	16	20	25	32
Groove valley diameter Ød <sup>1)</sup>	12,02	15,02	18,92	23,62	30,42
Ball center PCD	14,8	17,8	22,1	27,6	33,2
Outer diameter ØD	13	16	20	25	32
Allowable outer diameter tolerance	0 -0,018		0 -0,021		
Hollow hole Øid	7	11	14	18	23

<sup>1)</sup> The groove valley diameter Ød must be the value where no groove is left after processing.

#### 3.3.7 Calculating average load

When the load on the spline nut varies, as in the case of the industrial robots with a work piece when moving forward and has itself arm weight only when moving backward, it is necessary to calculate the life considering the conditions of variation of the load.

Average load (Pm) is a certain load that has the same life as the life under the conditions of this variable load when the load acting on the spline nut varies with various motion conditions.

The basic formula is shown below:

Formula 3.11

$$P_{m} = \sqrt[3]{\frac{1}{L} \times \sum_{n=1}^{n} (P_{n}^{3} \times L_{n})}$$

 $P_m$ : Average load (N)

- $P_n$ : Variable load (N)
- L: Total running distance (mm)
- L<sub>n</sub>: Distance traveled during P<sub>n</sub>

#### 3.3.8 The case of step load

Formula 3.12

$$P_{m} = \sqrt[3]{\frac{1}{L}} \times (P_{1}^{3} \times L_{1} + P_{2}^{3} \times L_{2} \dots + P_{n}^{3} \times L_{n})$$

- P<sub>m</sub>: Average load (N)
- $P_n$ : Variable load (N)
- L: Total running distance (mm)
- L<sub>n</sub>: Distance traveled during P<sub>n</sub>



#### 3.3.9 The case of linear variation

Formula 3.13

$$P_{m} = \frac{1}{3}(P_{min} + 2 \times P_{max})$$
$$P_{min}: Minimum load (N)$$

P<sub>max</sub>:Maximum load (N)

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## 3.3.10 The case of sinusoidal loading

Formula 3.14

 $P_m \coloneqq 0.65 \times P_{max}$ 

Formula 3.15

 $P_m \coloneqq 0,75 \times P_{max}$ 



# 4 Selecting preload

The preload of the ball spline significantly influences accuracy, and stiffness, so it is necessary to select the appropriate clearance (or preload) for the application. Clearance values are specified for each model number and can therefore be selected appropriately according to the conditions of use.

#### **Preload and stiffness**

Preload is a load applied to the ball beforehand to eliminate clearance in the rotation direction and improve stiffness. When preload is applied, the ball spline increases stiffness according to the strength of the preload. Fig. 4.1 shows the displacement in the direction of rotation when applying a rotational torsion.

As shown in Fig. 4.1, the effect of preload is maintained up to 2,8 times the preload load. Compared with the time without preload, the displacement becomes one-half of the same torsion and the stiffness is more than 2 times.





### 4.1 Conditions and benchmarks for use in the selection of preload

<u>Table 4.1</u> indicates the benchmarks for selection of clearance in the direction of rotation according to the conditions of use of the ball spline.

Clearance in the direction of rotation of the ball spline significantly influences the accuracy or stiffness of the ball spline. Therefore, it is important to select the appropriate clearance according to the application. Generally, products with preload are used. There is a high vibration shock in the case of a repeated rotating motion or a reciprocating linear motion, so applying preload will significantly improve the stiffness and accuracy.

|--|

Clearance in the direction of rotation	Conditions of use	Typical Applications
No preload	<ul> <li>Where it is intended to drive smoothly with a small force</li> <li>Where the torsion always acts in a certain direction</li> </ul>	<ul> <li>Various metering instruments</li> <li>Automatic drawing machine</li> <li>Shape measuring instruments</li> <li>Dynamometer</li> <li>Winding machine</li> <li>Automatic welding machine</li> <li>Boring and grinding machine main shaft</li> <li>Automatic packing machine</li> </ul>
Light preload	<ul> <li>Where the cantilever load or moment is applied</li> <li>Where high accuracy of repetition is required</li> <li>Where load is applied</li> </ul>	<ul> <li>Rocker arm of industrial robots</li> <li>Various automatic loading and unloading machines</li> <li>Automatic coating guide shaft</li> <li>Electric discharge machine main shaft</li> <li>Stamping die guide shaft</li> <li>Drilling machine main shaft</li> </ul>
Medium preload	<ul> <li>Where high stiffness is required and vibration shock is prone to occur.</li> <li>Where a spline nut is subject to the moment</li> </ul>	<ul> <li>The steering shaft of construction vehicles</li> <li>Paste welding machine shaft</li> <li>Automatic plate tool table indexing shaft</li> </ul>

#### Table 4.2: Clearance and preload range for each specification in the direction of rotation

Shaft diameter	No preload	Light preload	Medium preload
13	~	0 ~ 0,02 C	0,05 C $\sim$ 0,07 C
16, 20	~	0 ~ 0,02 C	0,05 C $\sim$ 0,07 C
25, 32	~	$0 \sim 0,02 \text{ C}$	0,05 C $\sim$ 0,07 C

C indicates basic rated dynamic load.

# 5 Selecting accuracy

#### 5.1 Linear ball splines

#### 5.1.1 Grade of accuracy

The grade of accuracy of the ball spline is expressed in terms of oscillation of the outer diameter of the spline nut against the supporting part of the spline shaft. It is divided into normal (C), high (H) and precision (P) which are shown in Fig. 5.1.

#### 5.1.2 Accuracy indication

RS type

Fig. 5.1: Measurement items of the accuracy of RS type ball spline



Table 5.1: Runout accuracy of	f RS type	ball splines
-------------------------------	-----------	--------------

Nominal shaft diameter/ Total length of spline shaft		13		16		20			25			32				
Above	Below	C	н	Р	С	н	Р	С	н	Р	С	н	Р	C	н	Р
-	200	56	34	18	56	34	18	56	34	18	53	32	18	53	32	18
200	315	71	45	25	71	45	25	71	45	25	58	39	21	58	39	21
315	400	83	53	31	83	53	31	83	53	31	70	44	25	70	44	25
400	500	95	62	38	95	62	38	95	62	38	78	50	29	78	50	29
500	630	112	-	-	112	-	-	112	-	-	88	57	34	88	57	34
630	800	-	-	-	-	-	-	-	-	-	103	68	42	103	68	42
800	1.000	-	-	-	-	-	-	-	-	-	124	83	-	124	83	-
	U	lnit µm														

#### Table 5.2: Geometric accuracy of RS type ball splines

	Shoulder vertic	ality (2)		Shoulder concentricity (3)				
Accuracy/ Nominal shaft diameter	C	н	Р	C	н	Р		
13	27	11	8	46	19	12		
16	27	11	8	46	19	12		
20	27	11	8	46	19	12		
25	33	13	9	53	22	13		
32	33	13	9	53	22	13		

Unit µm

• FS type

#### Fig. 5.2: Measurement items of the accuracy of FS type ball spline



#### Table 5.3: Runout accuracy of FS type ball splines

Nominal shaft diameter/ Total length of spline shaft		13		16		20		25			32					
Above	Below	C	н	Р	C	н	Р	C	н	Р	С	н	Р	C	н	Р
-	200	56	34	18	56	34	18	56	34	18	53	32	18	53	32	18
200	315	71	45	25	71	45	25	71	45	25	58	39	21	58	39	21
315	400	83	53	31	83	53	31	83	53	31	70	44	25	70	44	25
400	500	95	62	38	95	62	38	95	62	38	78	50	29	78	50	29
500	630	112	-	-	112	-	-	112	-	-	88	57	34	88	57	34
630	800	-	-	-	-	-	-	-	-	-	103	68	42	103	68	42
800	1.000	-	-	-	-	-	-	-	-	-	124	83	-	124	83	-

Unit µm

#### Table 5.4: Geometric accuracy of FS type ball splines

	Shoulder ver	rticality (2)		Shoulder co	n <mark>centricity (3</mark> )		Verticality (4)			
Accuracy/ Nominal shaft diameter	C	Η	Ρ	С	Н	Ρ	C	Η	Ρ	
13	27	11	8	46	19	12	39	16	11	
16	27	11	8	46	19	12	39	16	11	
20	27	11	8	46	19	12	39	16	11	
25	33	13	9	53	22	13	39	16	11	
32	33	13	9	53	22	13	39	16	11	

Unit µm

O FSR type



Fig. 5.3: Measurement items of the accuracy of FSR type ball spline

Table 5.5: Runout accuracy of FSR type ball splines

Nominal shaft diameter/ Total length of spline shaft		16			20			25			32			
Above	Below	C	Н	Ρ	C	Н	Р	C	Н	Р	C	н	Ρ	
-	200	56	34	18	56	34	18	53	32	18	53	32	18	
200	315	71	45	25	71	45	25	58	39	21	58	39	21	
315	400	83	53	31	83	53	31	70	44	25	70	44	25	
400	500	95	62	38	95	62	38	78	50	29	78	50	29	
500	630	112	-	-	112	-	-	88	57	34	88	57	34	
630	800	-	-	-	-	-	-	103	68	42	103	68	42	
800	1.000	-	-	-	-	-	-	124	83	-	124	83	-	
	U	Init µm												

Table 5.6: Geometric accuracy of FS	SR type	ball splines
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	Shoulder	verticality	(2)	Shoulder concentricity (3)			Outer ring	verticality	(4)	Outer ring yaw (5)			
Accuracy/ Nominal shaft diameter	C	Η	Ρ	C	Η	Ρ	C	Η	Ρ	C	Η	Ρ	
16	27	11	8	46	19	12	29	18	13	32	21	16	
20	27	11	8	46	19	12	29	18	13	32	21	16	
25	33	13	9	53	22	13	32	21	16	32	21	16	
32	33	13	9	53	22	13	32	21	16	32	21	16	

Unit µm

## 5.2 Compound ball splines

#### 5.2.1 Accuracy specifications

The compound ball spline consists of a ball screw nut and a ball spline nut, and is made according to the following specifications and inspected in accordance with Fig. 5.4 and Table 5.7.

- Ball screw
   Axial clearance: 0
   Lead accuracy: C4 grade
- Ball spline Clearance in the direction of rotation: 0 (light preload) Precision grade: H grade

#### Fig. 5.4: Measurement items of the accuracy of compound ball spline



### Table 5.7: Table of geometric accuracy of the linear ball spline

	Nominal shaft diameter	Ball screw nut		Ball spline nut					
		Verticality (1)	Runout (2)	Verticality (3)	Runout (4)				
	16	16	20	18	21				
	20	16	20	18	21				
	25	18	24	21	21				
	32	18	24	21	21				
	Unite come								

Unit µm

# 6 Dimensions of the ball spline

# 6.1 Linear ball spline RS, FS, FSR types

### 6.1.1 Product dimensions

RS type



Nominal shaft diameter	Basic rate	Basic rated load		Basic rated torsion		Outer diameter	Length	Keyway width	Keyway depth	Keyway length	Lubrication hole
	C (kN) $C_0$ (kN)		$\mathbf{C}_{\tau}$ (Nm)	<b>C</b> <sub>οτ</sub> (Nm)	MA (Nm)	D	L	b H8	$t_0^{+0,1}$	I <sub>0</sub>	<b>d</b> <sub>0</sub>
13	4,07	5,99	5,98	10,88	19,6	24	36	3	1,5	15	1,5
16	7,2	13,5	32,1	34,4	67,6	31	50	3,5	2,0	17,5	2
20	10,4	20,0	57,8	63,2	118	35	63	4	2,5	29	2
25	15,4	27,5	106,5	108,8	210	42	71	4	2,5	36	3
32	20,5	34,4	181,5	173,1	290	49	80	4	2,5	42	3

Unit µm

O FS type



Nominal shaft diameter	Basic rat	ed load	Basic rate	ed torsion	Allowable static torque	Outer diameter	Flange outer diameter	Length	Z1	Lubrication hole	W	m1	m2 × t1
	C (kN)	<b>C</b> <sub>0</sub> (kN)	$\mathbf{C}_{\tau}$ (Nm)	<b>C</b> <sub>οτ</sub> ( <b>Nm</b> )	MA (Nm)	D	F	L		<b>d</b> <sub>0</sub>			
13	4,07	5,99	5,98	10,88	19,6	24	44	36	7	1,5	33	4,5	8 × 4,4
16	7,2	13,5	32,1	34,4	67,6	31	51	50	7	2	40	4,5	8 × 4,4
20	10,4	20,0	57,8	63,2	118	35	58	63	9	2	45	5,5	9,5 × 5,4
25	15,4	27,5	106,5	108,8	210	42	65	71	9	3	52	5,5	9,5 × 5,4
32	20,5	34,4	181,5	173,1	290	49	77	80	10	3	62	6,6	11 × 6,5
	I	Jnit µm											

FSR type



Complexity       Complexity       Complexity       MAm       P       A1       L <thl< th=""> <thl< thr="">       L       L       &lt;</thl<></thl<>	inal Basic rated Basic ra t load torsion neter	c rated Allow- Outer able dia- static meter torque	Flange Total F1 outer Length dia- meter	<sup>-1</sup> S1	T1	E1	Z1	W	W1	m1 × t1	C1	Lubri- cation hole	Outer basic load	ring rated
<b>16</b> 7,2 13,5 32,1 34,4 67,6 48 64 50 36 31 21 10 6 56 30 M4 × 6 4,5 1,5 9,3 1	C C <sub>0</sub> C <sub>τ</sub> (kN) (kN) (Nm)	C <sub>or</sub> MA D (Nm) (Nm)	A1 L									<b>d</b> <sub>0</sub>	C <sub>a</sub> (kN)	C <sub>0a</sub> (kN)
	<b>6</b> 7,2 13,5 32,1	2,1 34,4 67,6 48	64 50 3	36 31	21	10	6	56	30	M4 × 6	4,5	1,5	9,3	11,5
<b>20</b> 10,4 20,0 57,8 63,2 118 56 72 63 43, 35 21 12 6 64 36 M5 × 8 4,5 1,5 9,8 13 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	<b>0</b> 10,4 20,0 57,8	7,8 63,2 118 56	72 63 4	43, 35 5	21	12	6	64	36	M5 × 8	4,5	1,5	9,8	13,3
<b>25</b> 15,4 27,5 106,5 108,8 210 66 86 71 52 42 25 13 7 75 44 M5 × 8 5,5 2,5 13,1	<b>5</b> 15,4 27,5 106,5	5,5 108,8 210 66	86 71	52 42	25	13	7	75	44	M5 × 8	5,5	2,5	13,1	22
<b>32</b> 20,5 34,4 181,5 173,1 290 78 103 80 63 52 25 17 8 89 54 M6×10 6,6 2,5 13,7 2	<b>2</b> 20,5 34,4 181,5	1,5 173,1 290 78	103 80 6	63 52	25	17	8	89	54	M6 × 10	6,6	2,5	13,7	25,2

Unit µm

#### **Compound ball spline FBR, FBL types** 6.2

#### **Product dimensions** 6.2.1



### Table 6.1: Dimensions for nut type FB: Ballscrew nut

Model	Specificat	tions		Ball s	Ball screw nut														Outer ring	
number	Nominal outer dia-	Nominal inner dia-	inal Lead r	Basic Ioad	rated	Outer diameter D2 g6	Flange outer diameter	Total length L2	F2 h7	<b>S2</b>	T2	E2	<b>Z2</b>	W2	W3	m2 × t2	C2	Lubri- cation hole	load	rated
	meter	meter		C (kN)	C <sub>0</sub> (kN)		AZ											<b>d</b> 1	C <sub>a</sub> C <sub>0a</sub> (kN) (kN)	
16	16	11	16	4,7	9,6	48	64	40	36,0	32	21	10	6	56	25	M4 × 8	4,5	1,5	9,3	11,5
20	20	14	20	6,4	14,0	56	72	46	43,5	40	21	11	6	64	31	M5 × 8	4,5	1,5	9,8	13,5
25	25	18	25	9,5	21,9	66	86	58	52,0	47	25	13	7	75	38	M6 × 12	5,5	2,5	13,1	22,0
32	32	23	32	13,0	29,8	78	103	72	63,0	58	25	14	8	89	48	M6 × 10	6,6	2,5	13,7	25,2

Unit mm

#### Table 6.2: Dimensions for nut type FB: Ballspline nut

Model	Ball spline nut															Outer ring				
number	Basic load	rated	Basic ra torsion	ited	Allowable static torque	Outer diameter D1	Flange diameter A1	Total length L1	F1 h7	<b>S1</b>	T1	E1	<b>Z</b> 1	W	W1	m1 × t1	<t1 c1="" th=""  <=""><th>basic load</th><th>rated</th></t1>		basic load	rated
	C (kN)	C <sub>0</sub> (kN)	C <sub>τ</sub> (Nm)	C <sub>οτ</sub> (Nm)	MA (Nm)													d0	C <sub>a</sub> (kN)	C <sub>0a</sub> (kN)
16	7,2	13,5	32,1	34,4	67,6	48	64	50	36,0	31	21	10	6	56	30	M4 × 6	4,5	1,5	9,3	11,5
20	10,4	20,0	57,8	63,2	118,0	56	72	63	43,5	35	21	12	6	64	36	M5 × 8	4,5	1,5	9,8	13,5
25	15,4	27,5	106,5	108,8	210,0	66	86	71	52,0	42	25	13	7	75	44	M5 × 8	5,5	2,5	13,1	22,0
32	20,5	34,4	181,5	173,1	290,0	78	103	80	63,0	52	25	17	8	89	54	M6 × 10	6,6	2,5	13,7	25,2

Unit mm

# 7 Design examples

#### 7.1 Inspection manual for the spline shaft design

For products that require the end machining of the spline shaft end, please check the following points when placing orders. The following Figure shows the basic drawing of the ball spline.

Fig. 7.1: Basic drawing of the ball spline



#### **Inspection requirements**

- a) Type of spline nut to be installed
- b) Number of spline nuts
- c) Clearance of rotating direction
- d) Accuracy
- e) With or without the dustproof ring
- Full length (whether the dimensions of all parts are ready and whether the total dimensions are correct)
- g) Effective length of the spline part
- h) Incomplete heat treatment area
- i) The direction of the flange (flange type)
- j) If spline shaft end part diameter is larger than stroke area.
- k) Position of the spline nut in relation to the shape of the spline shaft end (keyway of the spline nut, flange hole)
- I) Indication of the chamfer
- m) The shape of the chamfer of the spline shaft end
- n) Application of hollow shaft
- o) O ring position
- p) Maximum length
- q) Whether there are other precedents

## 7.2 Position of the keyway and flange hole of the spline nut

Among all types of ball splines, the keyway in the outer diameter of the spline nut is shown in Fig. 7.2 and is machined according to the position of the ball circulation.

In addition, the flange holes in the flange-type nuts are in the position shown in Fig. 7.3. Specify the position of the processed keyway, etc., on the spline shaft when placing orders.

Fig. 7.2: Position of the spline groove for RS type



SP13-RS type and smaller types

SP16-RS type and larger types

Fig. 7.3: Position of spline flange hole for FS type



SP13-FS type and smaller types

SP16-FS type and larger types

# 8 Installation steps

- 1 Recommended tolerance for spline nut mounting surface. When specifying the tolerance for the diameter of the mounting surface for the spline nut bracket, it is generally recommended to use a transition fit (J6) for best accuracy. However, a clearance fit (H7) may be used in cases where accuracy requirements are lower.
- 2 Examples of installation of the ball spline

Examples are shown in the table below. Although the tightness demand of the ball spline assembly does not need to be very high, it is important to avoid installing them without fixing them.

Table 8.1: Examples of installation of the ball spline



3 Installation of the ball spline nut

When installing the spline nut into the mounting surface, insert it slowly using the installation jig without hitting the C ring or the dustproof ring.

Fig. 8.1: Schematic diagram of installing the jig



Table 8.2: Recommended jig dimensions

Nominal shaft diameter	13	16	20	25	32
Di	11,5	14,5	18,5	23	28

4 Installation of the ball spline shaft

When inserting the spline shaft into the spline nut, take care to insert the spline shaft perpendicular to the spline nut insert the straight groove of the spline shaft along the positing guide part of the retainer or the dustproof ring. Do not force the spline nut in to avoid the balls falling out of the retainer.

If the spline nut is equipped with a dustproof ring or preloaded, lubricate the outer diameter of the spline shaft with lubrication grease in advance.

# 9 Option of ball spline

#### Lubrication

The lubrication varies depending on the conditions of use, but in general, the grease should be replenished at a running distance of 100km (6 months~1 year). Lubricate the spline shaft by applying grease to the rolling groove or injecting grease into the nut lubrication hole, as shown in Fig. 9.1.

Fig. 9.1: Lubrication method



#### Material and surface treatment

Depending on the conditions of use, the ball spline may be treated by rust prevention or be manufactured with different material. Please contact HIWIN for the rust prevention treatment and change of material used.

# 10 Precautions for use

#### Transportation/Assembly

- 1 When transporting heavy products (20kg or more), two or more people or transporting equipment is requested. Otherwise, it may result in scratches or damage.
- 2 Do not disassemble any part. Otherwise, it may result in loss of function.
- 3 The spline nut and spline shaft may fall by their weight when tilting, so be careful.
- 4 Do not allow the ball spline to fall or be impacted. Otherwise, it may result in scratches or damage. In addition, even if the damage is not visible from the outside, it may result in loss of function if it is hit.
- 5 When assembling, do not remove the spline nut from the spline shaft.
- 6 When using the product, wear protective gloves, safety shoes, etc., as necessary to ensure safety.

#### **Precautions for use**

- 1 Please take care to prevent the inflow of foreign objects into the nut such as particles and coolant. Otherwise, it may result in damage.
- 2 When using the product in an environment where particles, coolant, corrosive solvents, water, etc. may flow into the product, use a soft telescopic sheath or dustproof cover to prevent them from flowing into the product.
- 3 Do not use at temperatures exceeding 80°C. Except for the heat resistant type, if the temperature is exceeded, it may cause deformation and damage to the resin and rubber parts.
- 4 If foreign objects such as metal shavings are attached, clean and lubricate again.
- 5 During short stroke application, it is difficult to form an oil film on the contact surface of rolling elements, and micro-abrasion may occur, so use a lubrication grease with high micro-abrasion resistance. In addition, it is recommended to form an oil film on the rolling elements periodically by applying a stroke of about the length of the spline nut.
- 6 Do not force the position parts (pins, keys, etc.) into the product. Otherwise, the rolling surface may become indented and may result in loss of function.
- 7 In case of misalignment or skewing of the supporting part of the spline shaft and spline nut, the service life will be extremely shortened. Please pay attention to the installation parts and installation accuracy.
- 8 If the spline nut is inserted into the spline shaft and used in the absence of the steel balls, premature damage may occur.
- 9 If any steel balls falls out of the spline nut, do not continue to use this product and contact HIWIN.
- 10 When installing the spline shaft into the spline nut, check the position in relation to the shaft and the spline nut while inserting the shaft into the spline nut without any inclination, since there is a comparison mark on the spline shaft and the spline nut. If it is inserted too forcibly, the balls may fall out. Please pay special attention. Apply lubricant to the outer diameter of the spline shaft when inserting the spline nut with a gasket or the preloaded spine nut.
- 11 When inserting the spline nut into the shaft, insert it slowly using a jig without hitting the side plate, end cap ring or gasket.
- 12 If the stiffness and accuracy of the installation components are not sufficient, the load on the bearing will be concentrated locally, and the performance of the bearing will be significantly reduced. Therefore, gives due consideration to the stiffness and accuracy of the support seat and base seat and the strength of the fixing screws.
- 13 Please contact HIWIN when machining positioning pin holes on the ball spline with flanges, etc. 34 S99TC01-2112

#### Lubrication

- 1 Wipe off the rust-proof oil carefully and lubricate before use.
- 2 Do not mix different lubricants together for use. Even lubricant greases with the same type of thickening agent may affect each other due to different additives, etc.
- 3 Use the lubricant grease that fits the specifications and environment if it is used in a special environment, such as a place where there is a lot of vibration, a clean room, vacuum, or low or high temperature.
- 4 When lubricating a product without a grease nipple or oil hole, apply lubricant directly to the rolling surface and make several test runs in order to inject the lubrication grease into the product.
- 5 The consistency of lubrication grease varies depending on the temperature. The sliding resistance of the ball spline changes due to the change in consistency, so please pay attention to it.
- 6 After adding lubrication grease, the mixing resistance of the lubrication grease may cause an increase in the sliding resistance of the ball spline. Make sure to carry out a test run and operate the machine after getting used to the lubrication grease.
- 7 After adding lubrication grease, excess lubrication grease may be dispersed to the surrounding area, so wipe it off before use if necessary.
- 8 The lubricant properties will deteriorate over time, so it is necessary to check and replenish the lubrication grease according to the frequency of use.
- 9 The lubrication interval varies depending on the conditions and environment of use. It is recommended to lubricate the system approximately every 100km travel distance (3-6 months). The final lubrication interval should be set according to the actual machine.
- 10 When lubricating with oil, sometimes the lubricant may not reach due to the installation direction of the ball spline. Please contact HIWIN in advance for details.

#### Storage

When storing the ball spline, place it in the HIWIN specified package and store it horizontally in the room to avoid high and low temperatures and high humidity. Since the internal lubricant will deteriorate over time, store the product for a long time, lubricate it again before use.

#### Disposal

Please discard the product as industrial waste as appropriate.